

Brownian Ground Motion And Dynamic Alignment of the Accelerator

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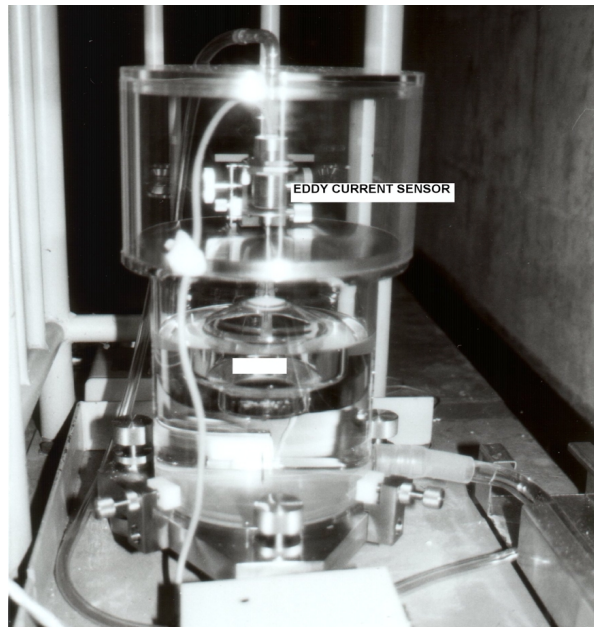
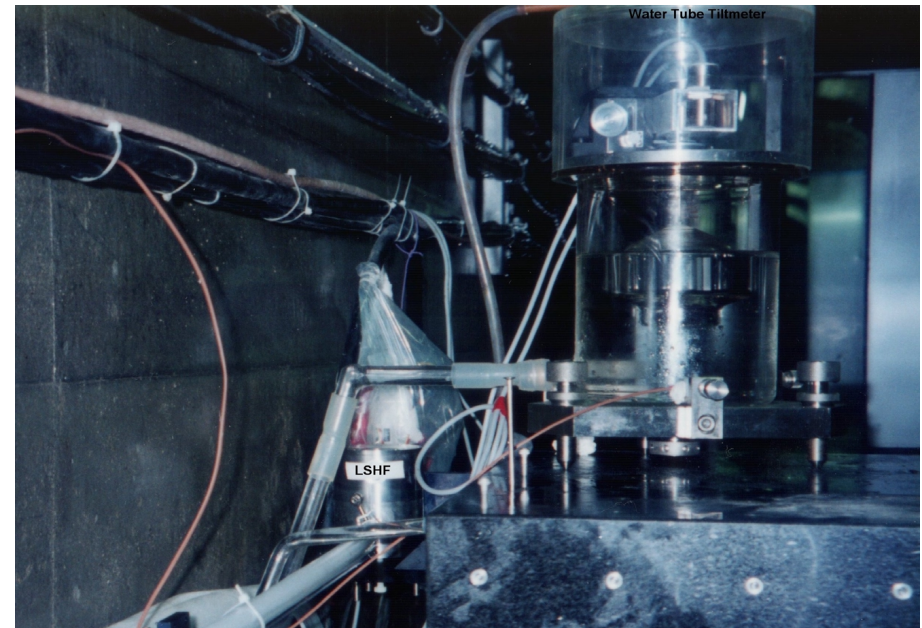
- **Power Spectrum Density and Coherence**
- **Slow Ground Motion and Geology**
- **Slow Ground Motion and Excavation Methods**

Typical Parameters of Linear Collider

		X-band	C-band	
Beam Energy Entrance/Exit	E_0/E_1	10/500	10/500	GeV
Particles/bunch	N	0.8	1.0	10^{10}
Invariant Emittance	ε_{N_y}	30	30	nm
Bunch length	σ_z	80	200	μm
β at entrance	β_0	4	4	m
Rf frequency	f	11.4	5.7	GHz
Accel. gradient	dE/ds	45	32	MeV/m
Iris radius/wavelength	a/λ	0.16	0.14	
ATL coefficient	A	1	1	$\text{nm}^2/\text{s}/\text{m}$
Stable time for $\epsilon = 0.1$	t	3	24	hours

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Sensors for Studies



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Empirical Continuous Power Spectrum Density ;

$$P(f) = \frac{K}{4\pi^2 f^2 (f_0^2 + f^2)}, \quad (1)$$

$f_0 : 0.1\text{Hz} - 0.01\text{Hz}$

In the hard rock region: $f_0 \approx 0.1\text{Hz}$

$$f = f_0 P(f) = K/f^2$$

Brownian motion of rocks becomes dominant

K strongly depends on the site

The ATL model:

Formulation using an auto-correlation function

$$\langle y(t+\tau)y(t) \rangle$$

$$\Delta y(\tau)^2 = 2 \langle y(t)^2 \rangle - 2 \langle y(t+\tau)y(t) \rangle = A \cdot L \cdot \tau. \quad (2)$$

$\langle X \rangle$: an ensemble average

Definition of a Power Spectrum;

$$P(f) = \int_{-\infty}^{\infty} \langle y(t+\tau)y(t) \rangle e^{-2\pi i f \tau} dt d\tau, \quad (3)$$

$$A \cdot L \cdot \tau = 4 \int_{-\infty}^{\infty} P(f) \sin^2(\pi f \tau) df. \quad (4)$$

$[f = f_0]$

$$4 \int_{-\infty}^{\infty} P(f) \sin^2(\pi f \tau) df = K \cdot \tau \quad (5)$$

Power Spectrum of ATL model as,

$$P(f) = \frac{A \cdot L}{4\pi^2 f^2}. \quad (6)$$

[Actual Experiment]

$$P(f) = \frac{K}{4\pi^2 f^2 + (1/\tau_{\max})^2}, \quad (7)$$

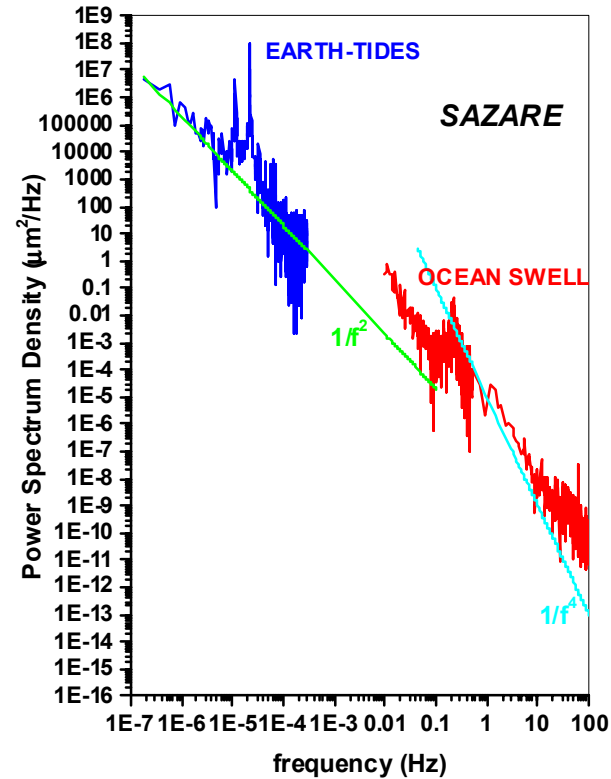
$1/\tau_{\max}$: cutoff frequency

The Integration of Equation (5);

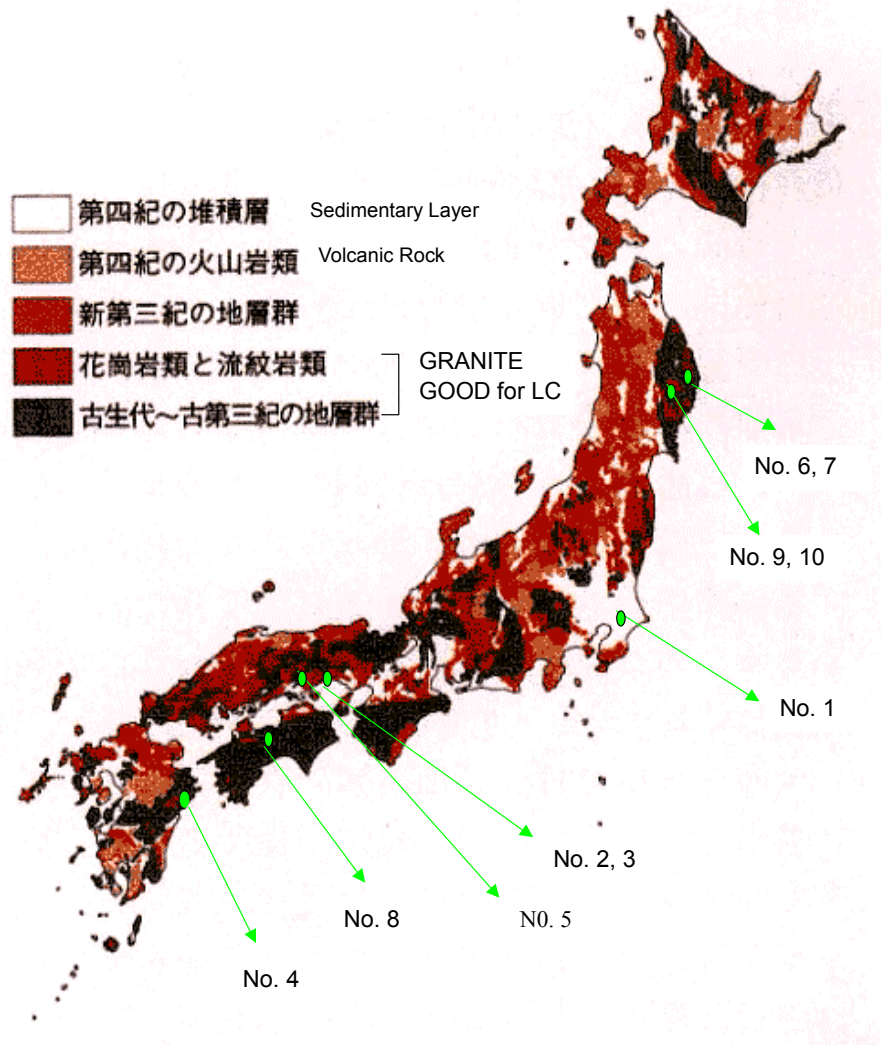
$$4 \int_{-\infty}^{\infty} P(f) \sin^2(\pi f \tau) df = K \tau_{\max} (1 - e^{-\tau/\tau_{\max}}). \quad (8)$$

[ATL Model]

$$\Delta y(\tau)^2 = A \cdot L \cdot \tau_{\max} (1 - e^{-\tau/\tau_{\max}}). \quad (9)$$



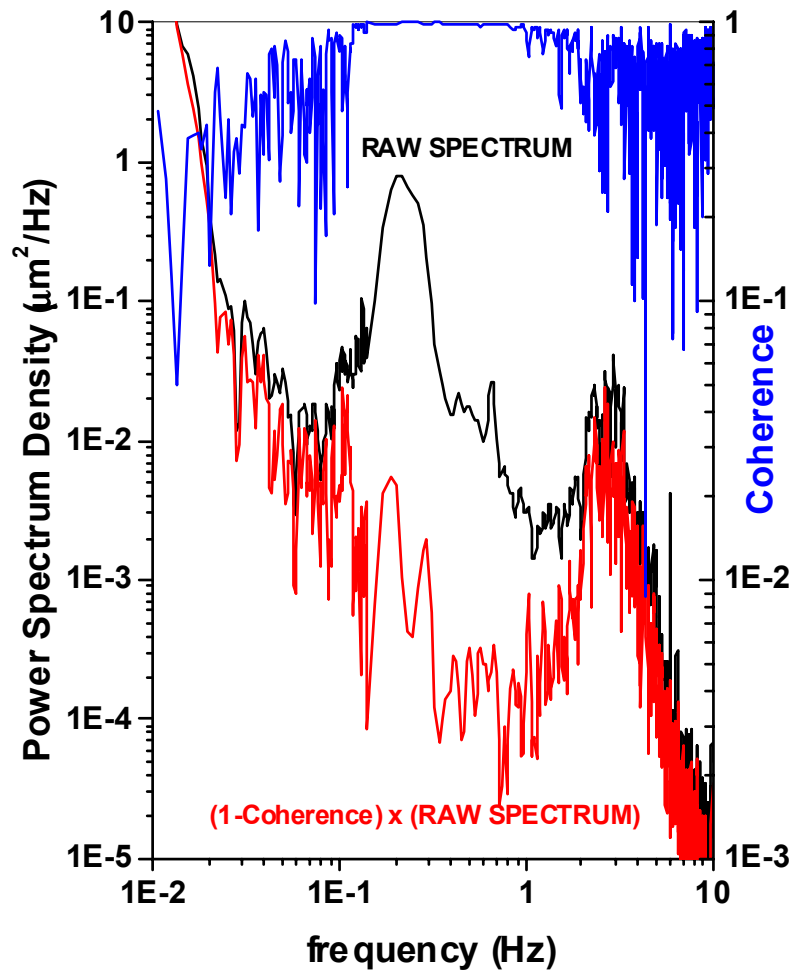
Recently, many accelerator physicists use ATL model for their accelerator simulation because of simplification of the calculation. But we have to take account of **applicable limitations in the light of coherency of the ground motion spectrum.**



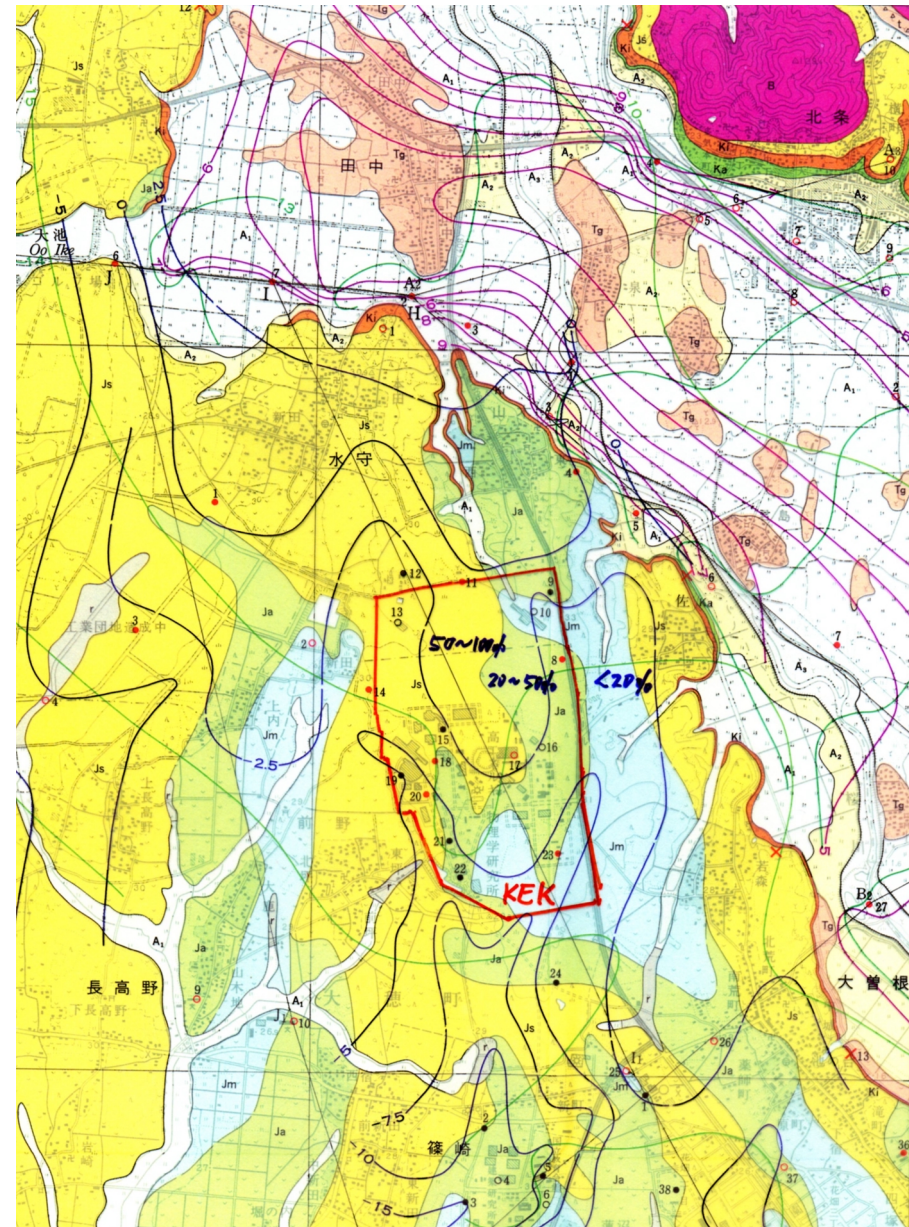
ATL COEFFICIENT in JAPAN			
No	Site Name	A (nm ² /m/sec)	Geology of the Site
1	Tunnel of KEKB	4.0E+01	Clay and Gravel
2	Rokkoh-1	3.6E+01	Granite (near Fault)
3	Rokkoh-2	3.3E+01	Granite
4	Miyazaki	1.5E+01	Diorite
5	Spring-8	8.0E-01	Granite
6	Kamaishi-1	1.4E-01	Granite (Crack and Water)
7	Kamaishi-2	5.7E-02	Granite
8	Sazare	5.0E-02	Green Schist
9	Esashi-1	5.7E-03	Granite (Floating Stone)
10	Esashi-2	2.0E-03	Granite

Geological Map of Japan and the Related Sites for ATL Table.

Described numbers are the same in figures and Table.



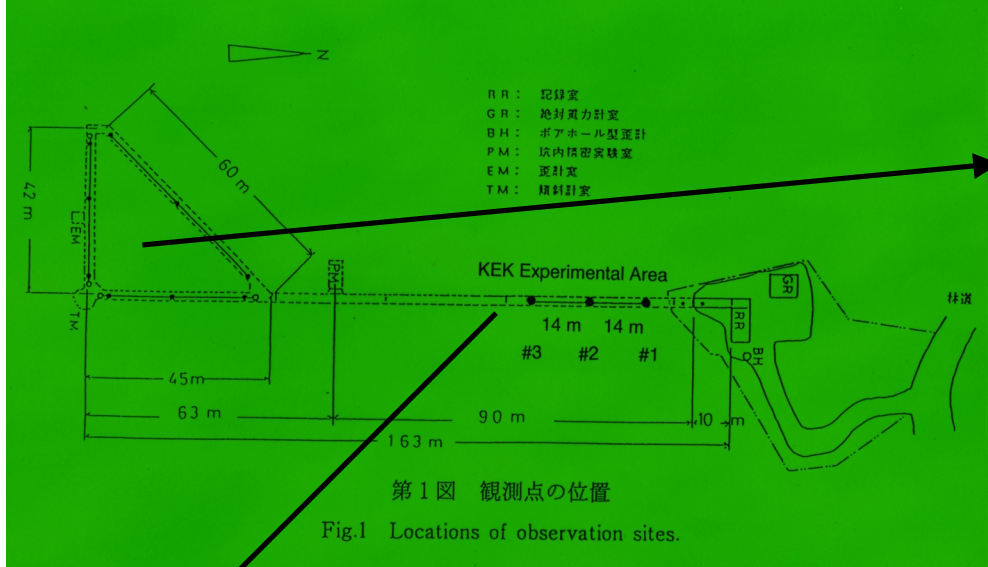
Ground motion in the noisy site (KEK). **Coherence** between two points at a distance of 48 m. Power spectra for the two points are the same. **Incoherent spectrum** is given by the equation shown in the figure. A big bump spectrum, around 0.2 Hz, corresponds to the ocean swell. The **incoherent spectrum** around 3 Hz comes from traffic noises. This incoherent vibration gives an amplitude of **83 nm**. That is, the tunnel in KEK should have a depth of 900 m, providing we want the amplitude of 1 nm.



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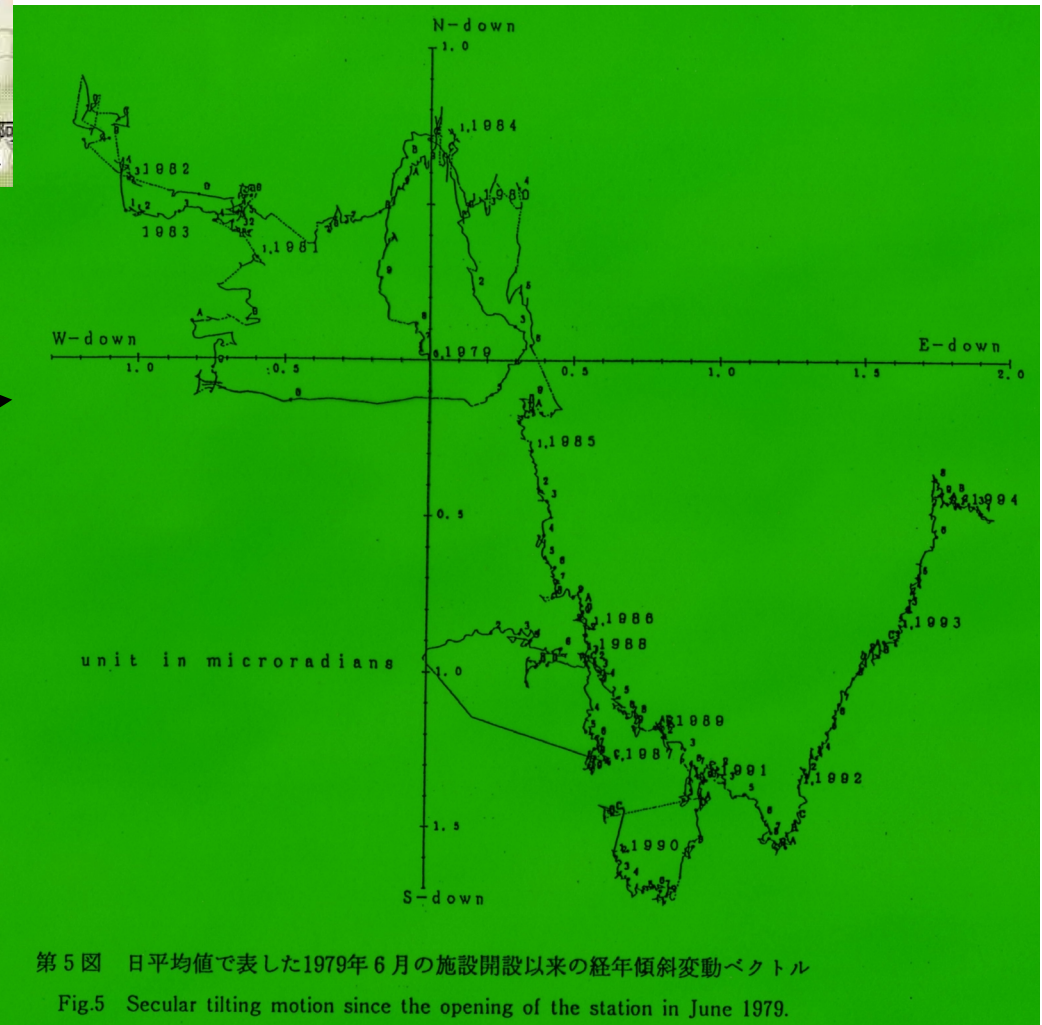


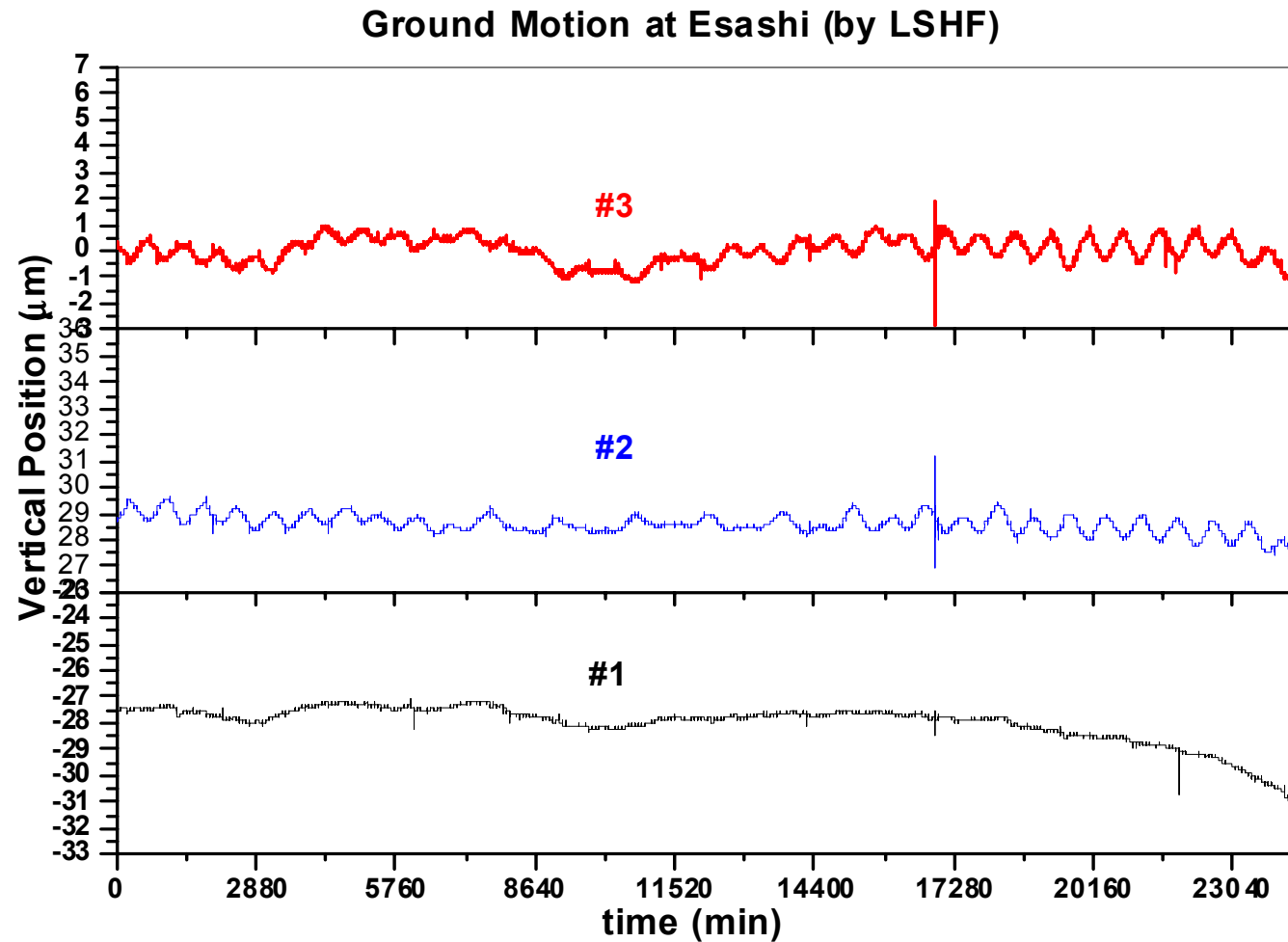
Esashi Earth Tides Station



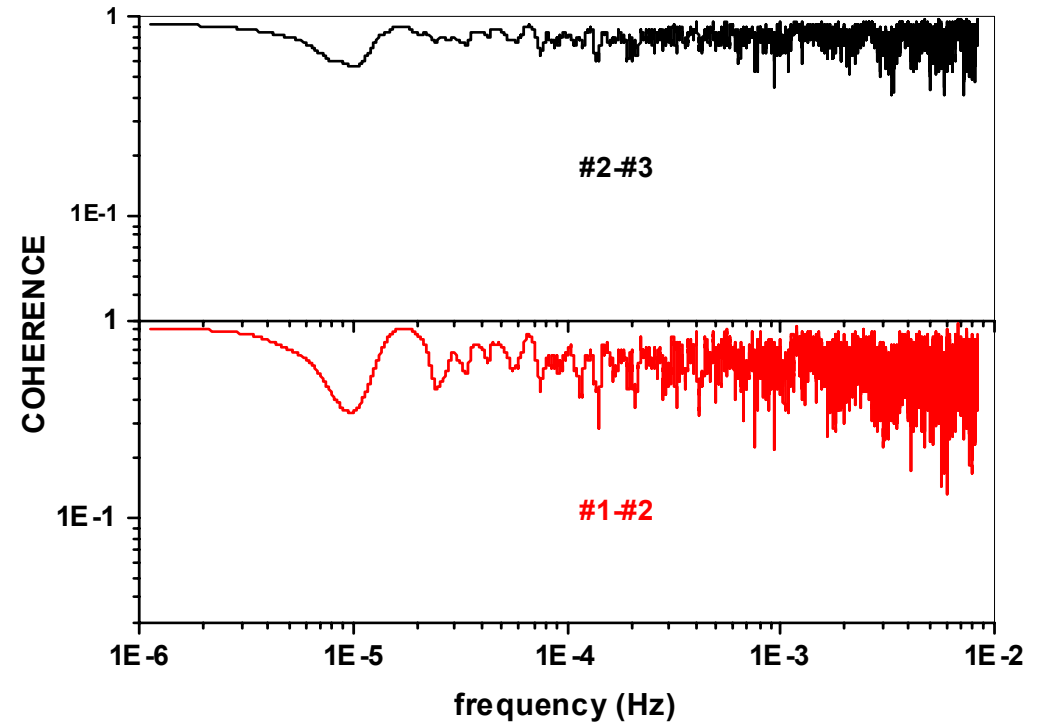
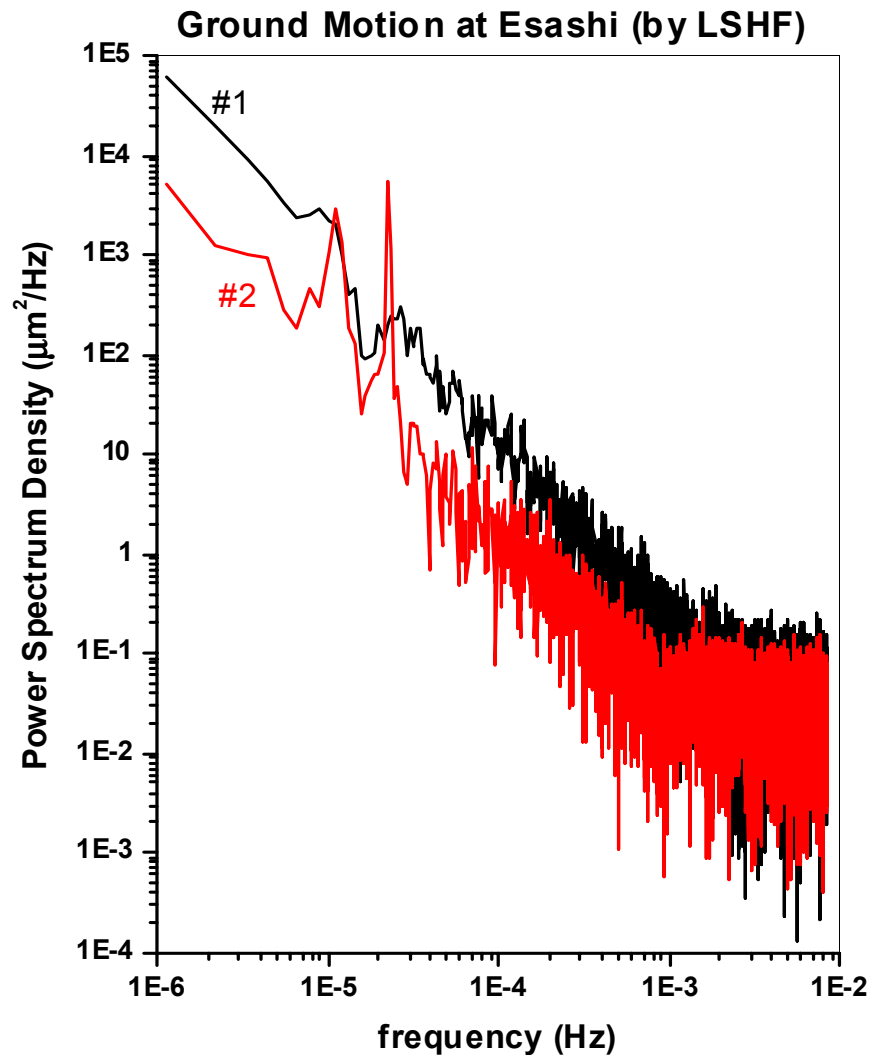
KEK観測施設(1994年～現在)

観測地点の詳細と長期間の傾斜変動観測例





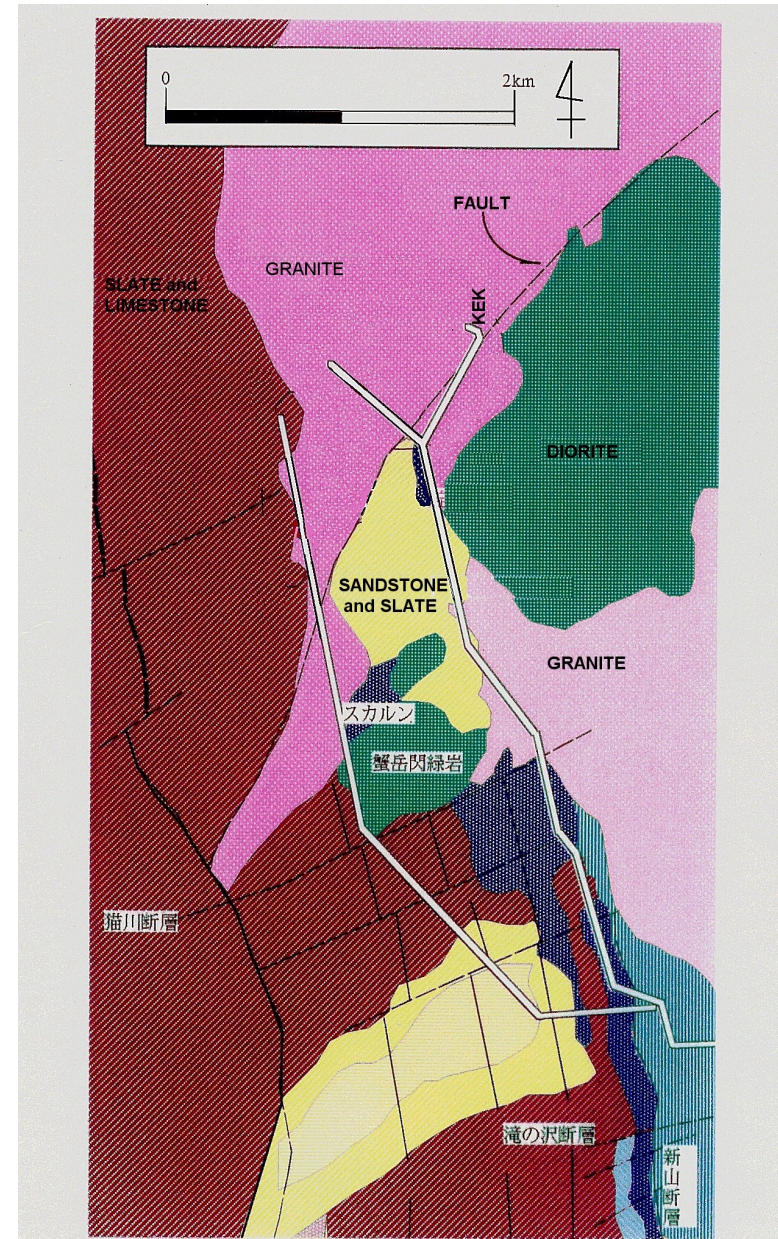
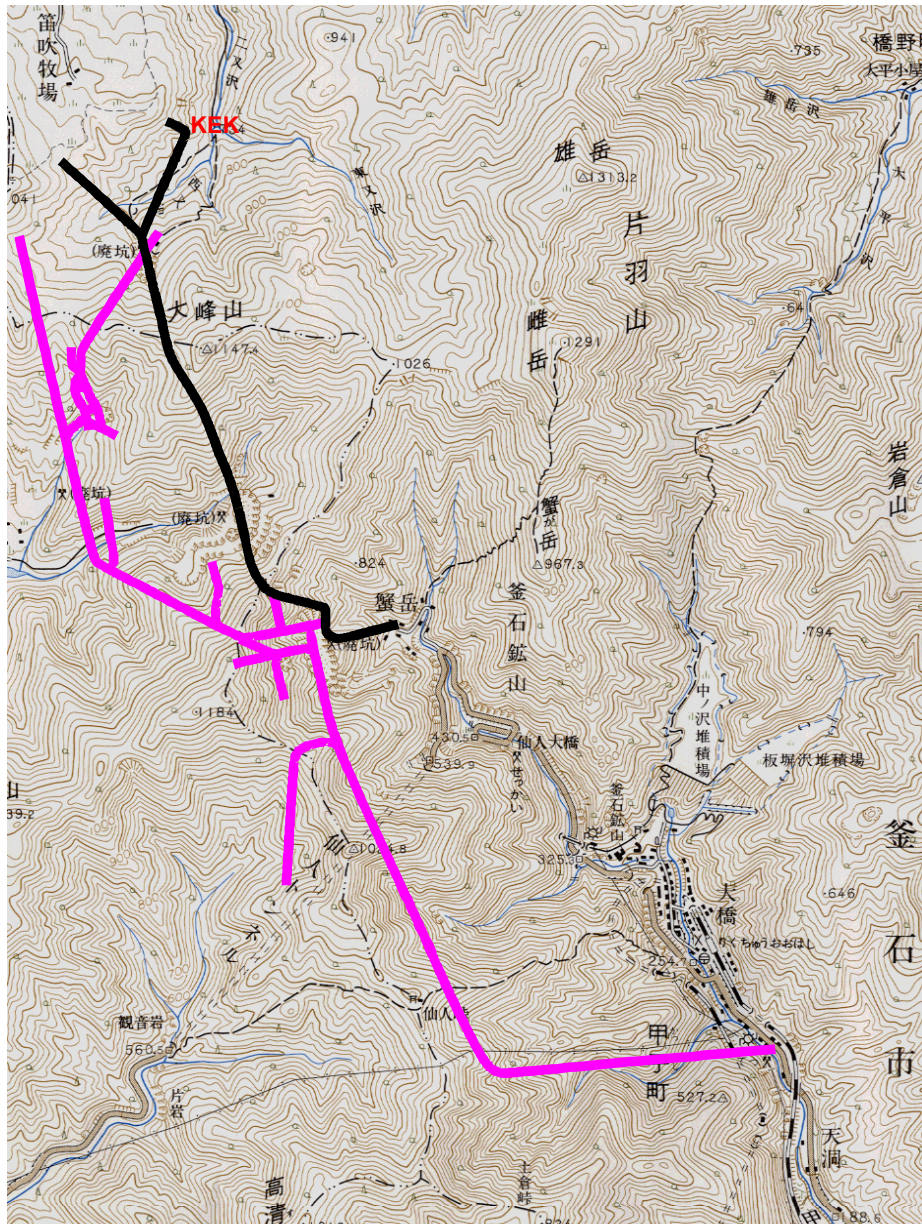
The time series data on the vertical ground motions observed at three points being 14 m apart between one another.



Coherence in the Granite Tunnel Having a Floating Lumped Rock.

Except the #1 lumped rock position, we get good coherence.

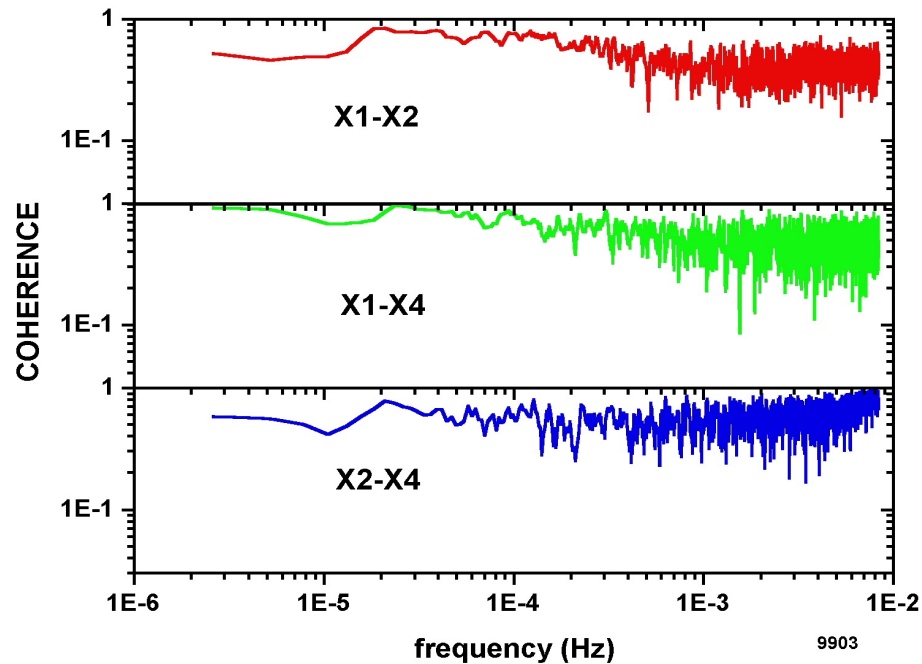
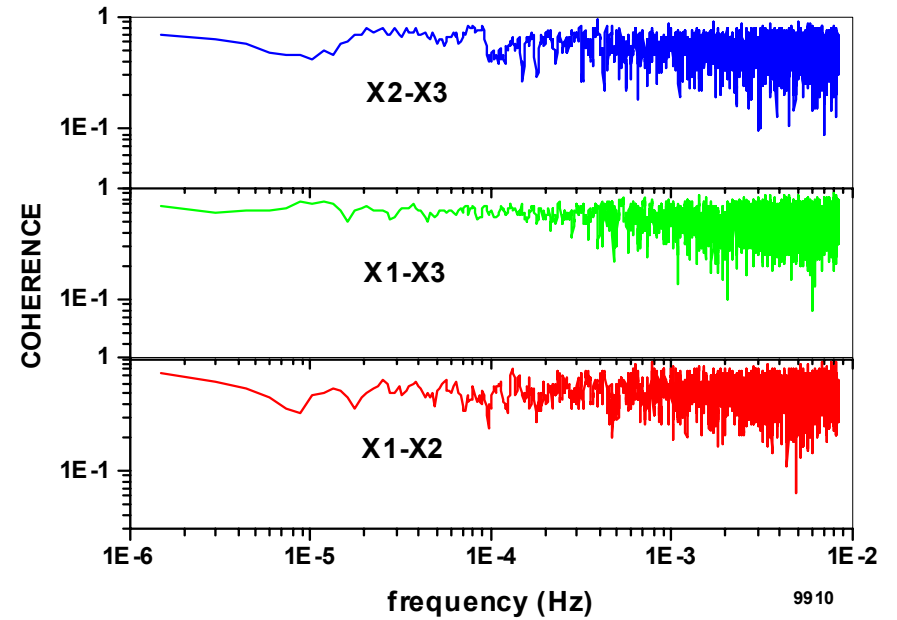
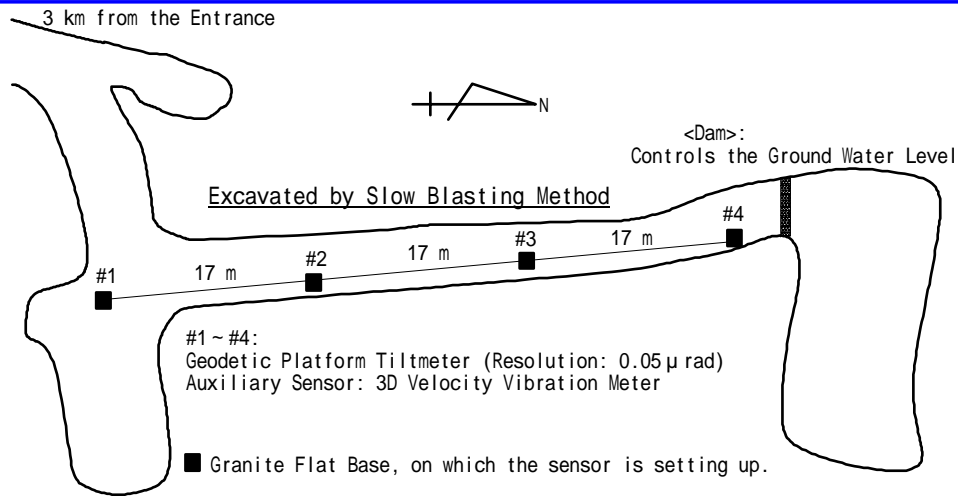
#1 shows no earth-tide spectrum. *ATL* coefficient in this point is a little bad as shown in the previous *ATL* Table.



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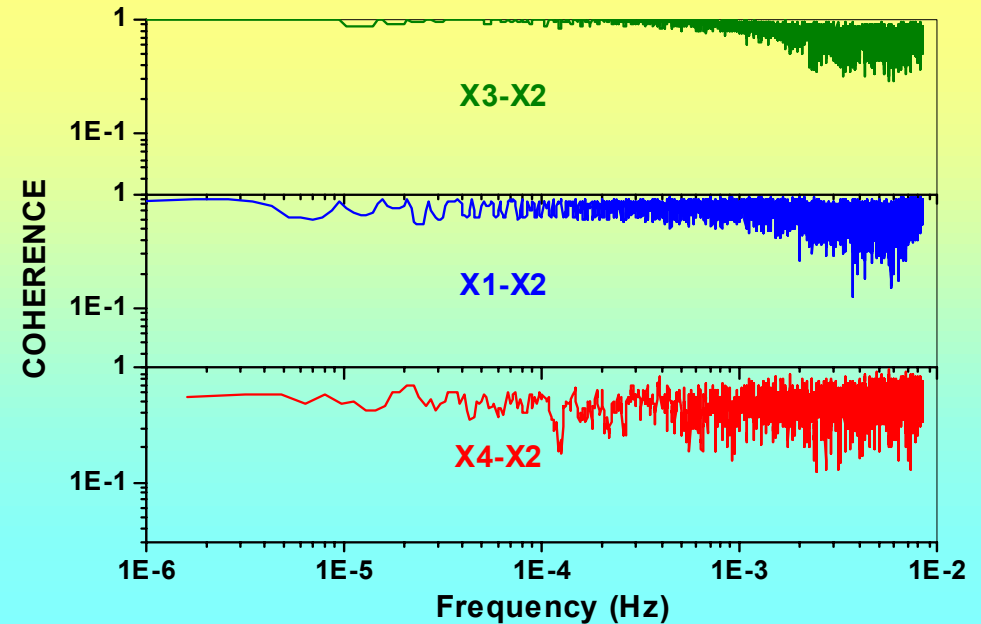
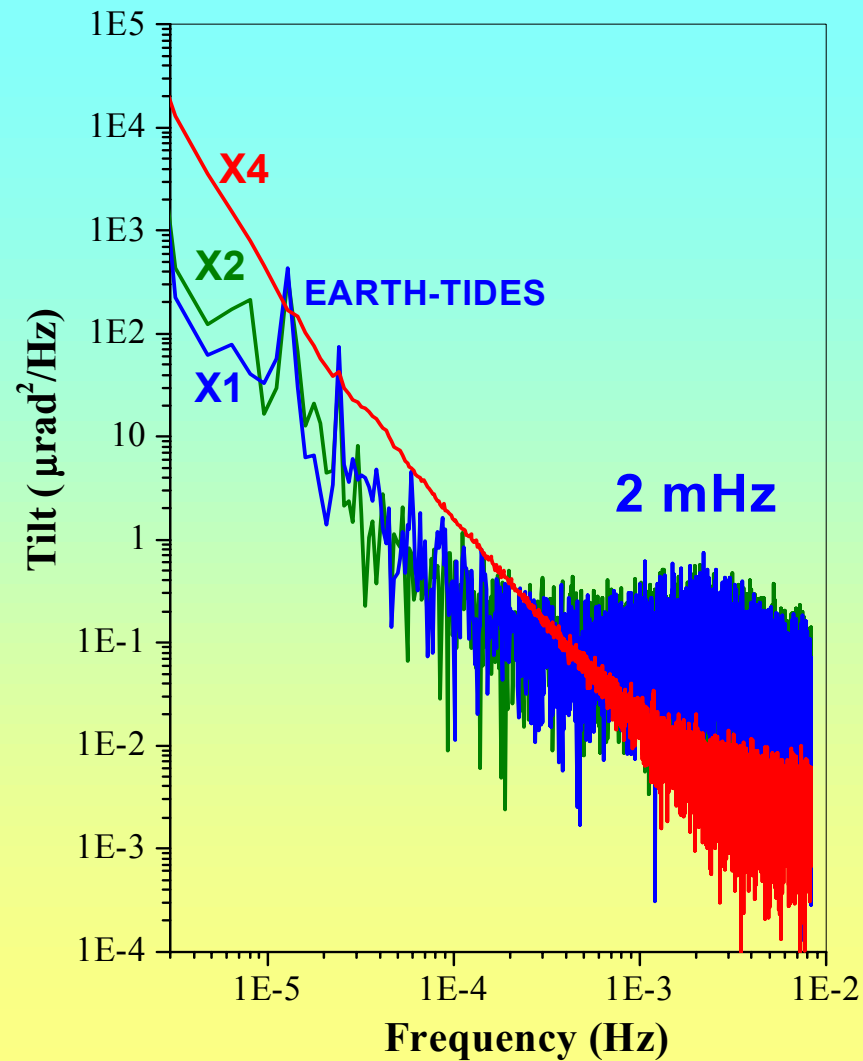
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Coherence-2



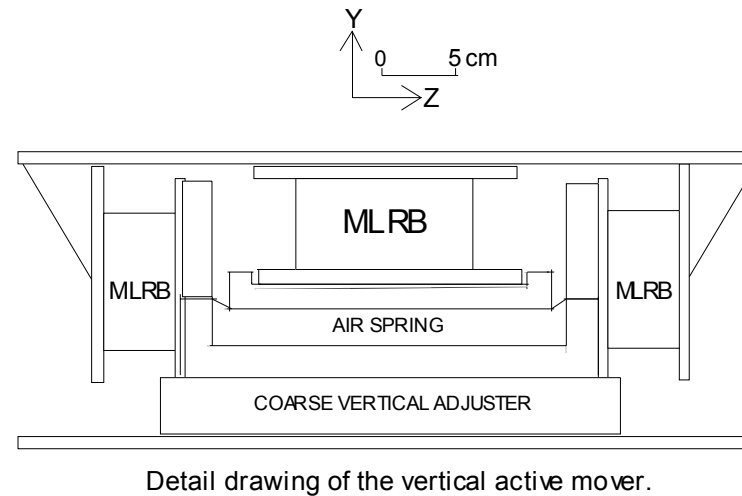
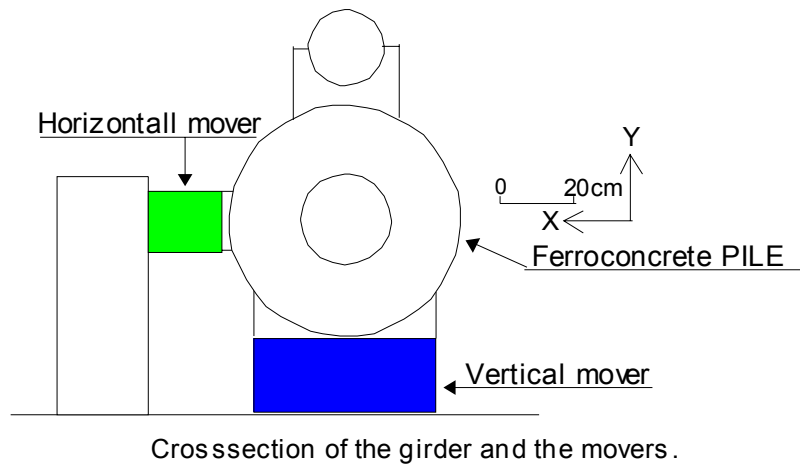
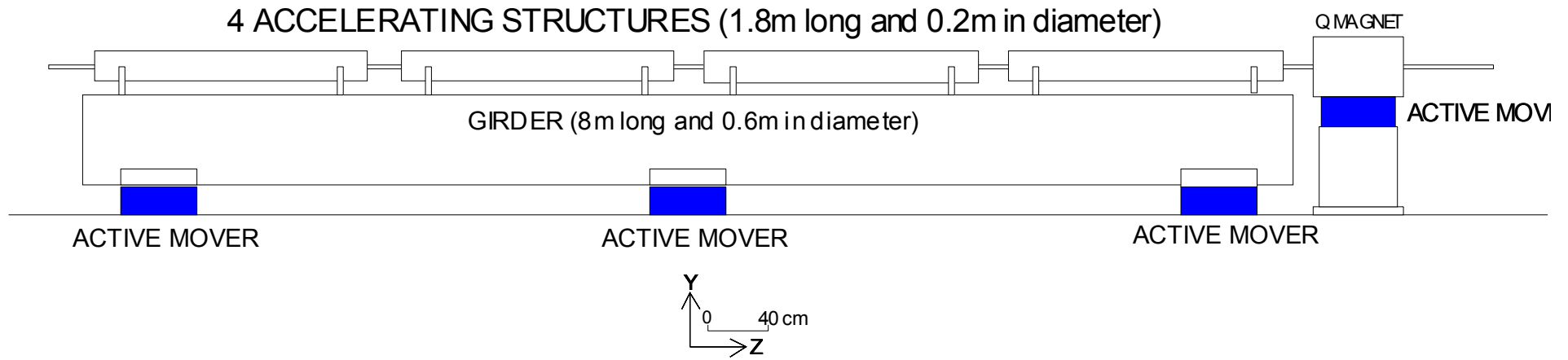
EFFECT of BLASTING CREVICE:

We executed several experiments to get detailed information about the surface layer of the granite tunnel cut by SBM. The coherence shows very complex changes without the dam.



In order to check the activity of underground water, we built a dam across the flow to control the water level in the crevice.

- #2 was mostly suffered by the reaction between the crevice and the water.
- #4 is another effect, such as lumped rock like Esashi.



架台の共振点：

X 軸方向： 5.8Hz、12.5Hz、16Hz、29Hz、

Y 軸方向： 12～16Hz のブロード共振、30Hz、90Hz、

Z 軸方向： 2.3Hz、5.6Hz、8Hz、80Hz、

ガーダーのクリープ特性と高剛性化

加速管： 長さ 1.8m

重量 250kg

使用数 8,000 台

設置精度 30 μm

ガーダー及び調整機構は 3 μm 以下の確度で再現性

コンクリートパイルの鋼板巻きの低価格ガーダーは、そのクリープ特性の評価が製作条件に強く依存して非常に困難であることが判明

強く伸張したピアノ線材（PC 鋼棒）をコンクリートで固めた円柱架台

クリープ歪み進行過程の計算：クリープの進行が 4 μm 以下になるのが製作後約一年掛かる。

表 - 1 ガーダー材料の諸元

材料	断面積 (cm ²)	断面 2 次モーメント (cm ⁴)	ヤング 率 (ton/cm ²)	単位長重 量 (kg/m)
PC 杭：600 , t=90	1,473	493,415	410	375
角形コラム：600 , t=16	363	203,000	2,100	285
RC：600	3,600	1,080,000	210	864

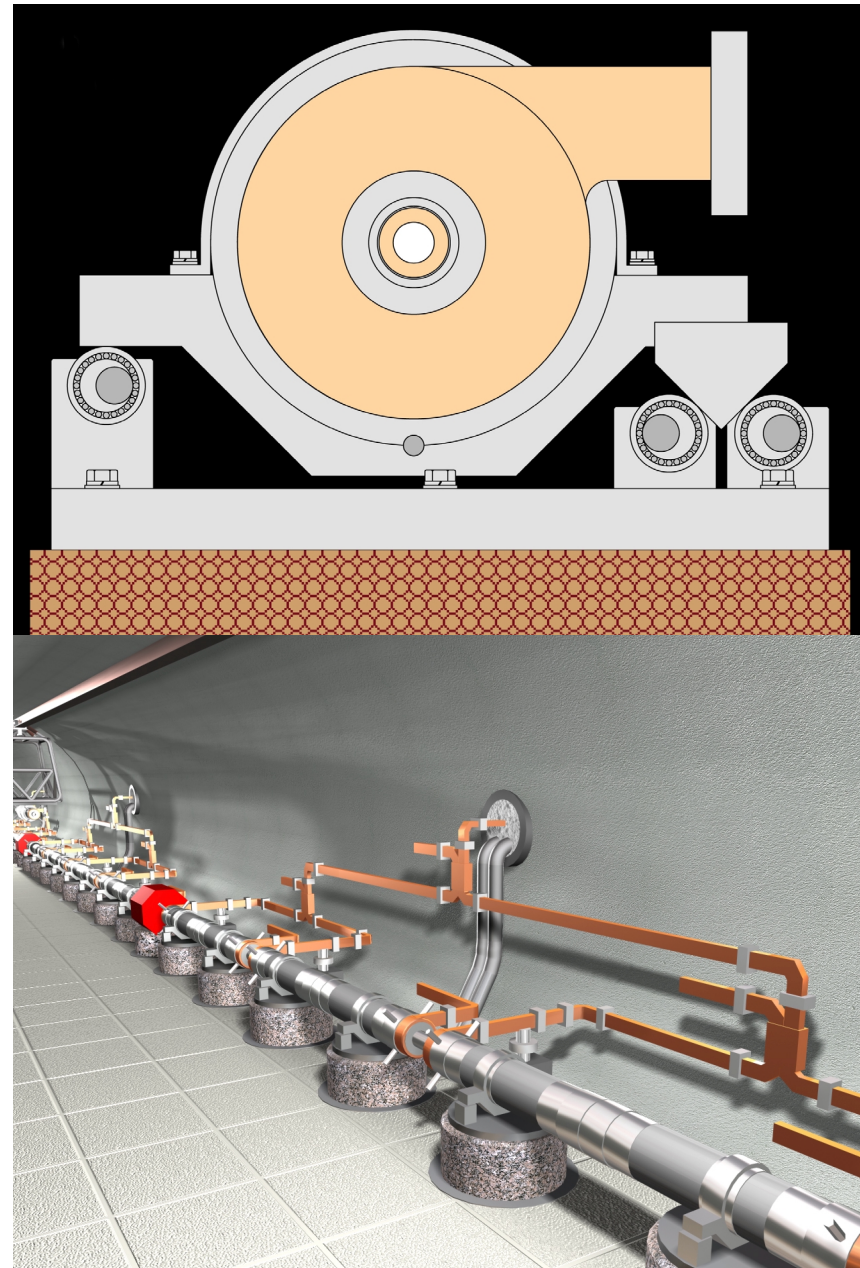
PC 杭は肉厚 90mm の円筒状とし、9 の PC 鋼棒を一樣に配置した。

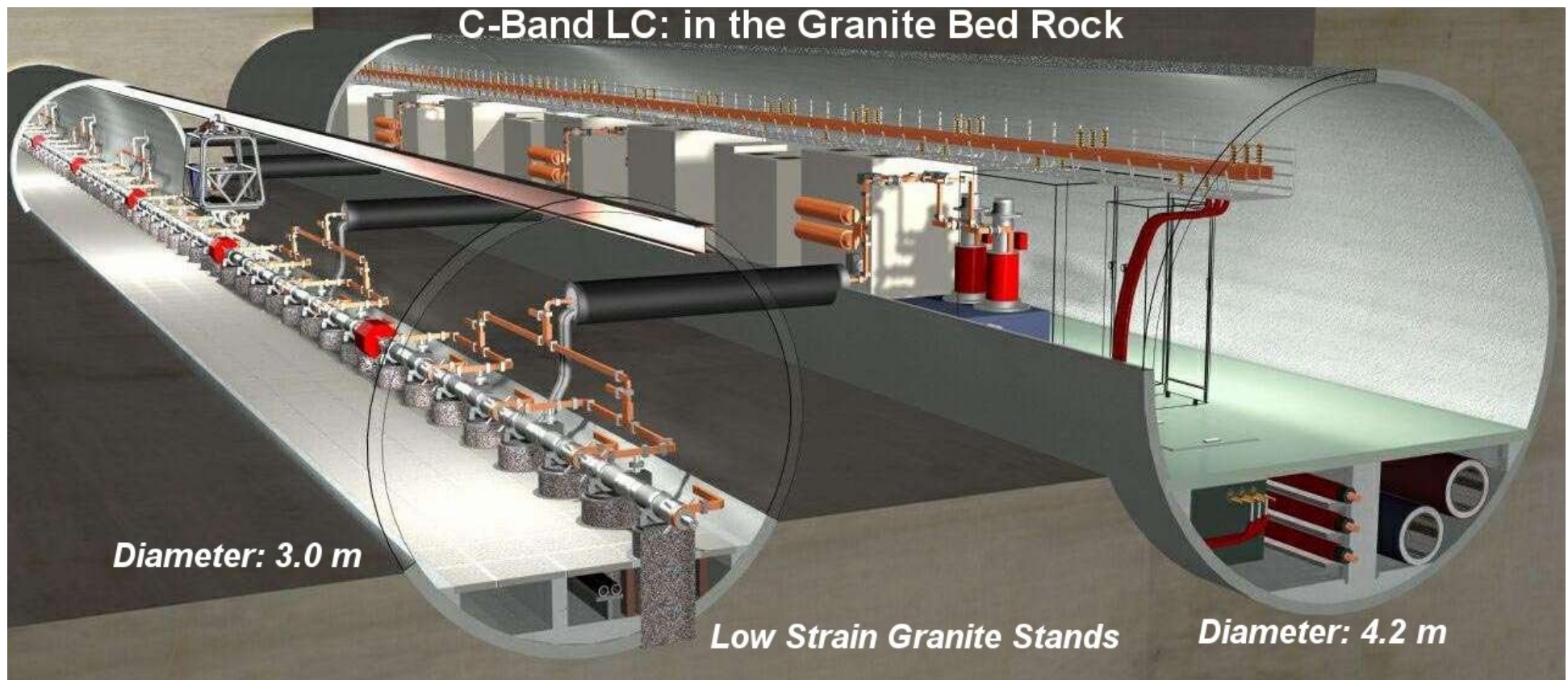
表 - 2 各ガーダー材料諸元に対する固有振動数 (Hz)

モード次数	1 次	2 次	3 次	4 次	5 次
モード形状	Y	Z	X	弾性モード	弾性モード
PC 杭	5.0	5.8	7.0	33.8	228.0
角形コラム	5.0	5.8	7.0	51.6	355.9
RC	5.0	5.9	7.1	26.7	175.7

以上から、RC 杭方式の代わりに、PC 杭を使う方が LC のガーダーとして有効であることが分かった。残る問題で解決せねばならないことは、

- 1) PC 杭方式の方が RC 杭方式に比べて、製作費が 3.5 倍になること、
- 2) 5 Hz の Y 方向振動に対するダンパーが必要なこと、
- 3) ガーダーの重量が 3 トンと重くなり、その分電動駆動機構の負荷が大きくなる。





- It is essential to search the site being $A < 1 \text{ nm}^2/\text{m}/\text{sec}$ for the long term stability of the alignment.
- TBM is the best solution for cutting the tunnel of LC.
- The separated tunnel is preferable to suppress the noises in the accelerator tunnel caused by the accelerator facility.
- We have to pay attention to local fluctuation of the ATL coefficient and the coherence around the betatron wave length for the construction of the long scale LC.